

Catalytic oxidation of VOC – modelling, reactor design and industrial off gas treatment

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Introduction & Methods

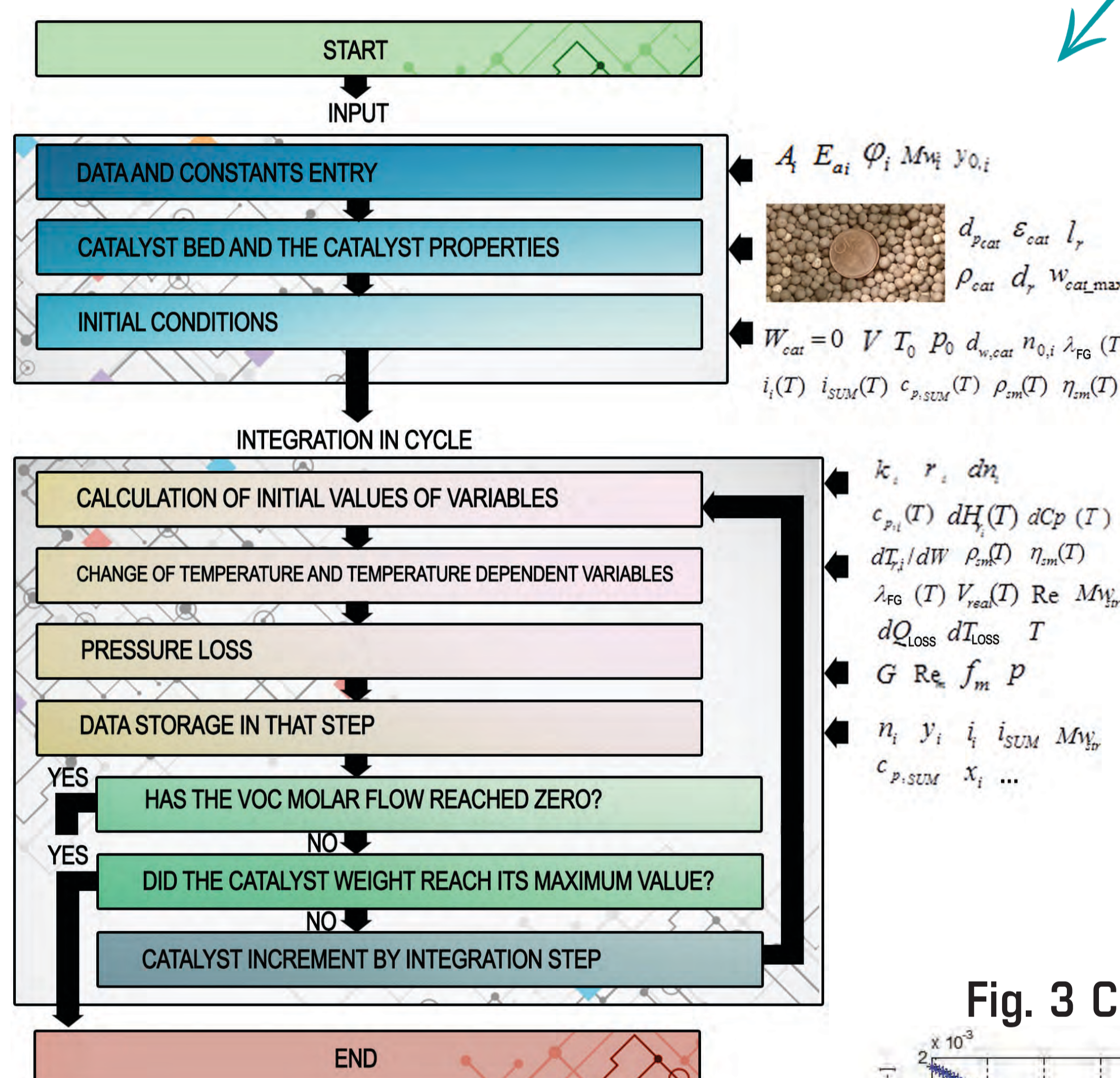
- Treatment of industrial off gas that contains VOC.
- Industry -> Frequently done by **thermal oxidation** by simply burning the VOC with NG.
- Often possible to change the technology -> **thermal OX** -> **catalytic OX** and reduce operating costs.
- Stable gas flow and no sudden changes in VOC concentration loads must be met to get reasonable reactor dimensions and IRR.
- Modelling of the process in pilot scale and fullscale -> the isothermal reactor can't be used, and instead, the adiabatic or even better, the non-isothermal reactor with heat dissipation should be considered.



- Proposed **MODEL** (considering non-isothermal plug-flow reactor) can predict the achievable conversion and temperature gradient across the reactor, which can help in reactor design, technological design of catalytic bed and scale-up to the full-scale technology.
- Proposed **MODEL** -> shows changes in gas composition and gas properties due to oxidation reactions, temperature rise due to oxidation reactions and on the other hand temperature decrease due to heat losses and change of pressure due to pressure losses across the bulk catalyst bed.
- Modular design **PILOT PLANT** was proposed and implemented -> verification of feasibility in industrial case studies of VOC catalytic oxidation and catalyst testing. This unit is scalable and can be used to test the sprinkled catalysts and monoliths both in lab or industrial conditions.

Results & Discussion

Fig. 1 Simplified diagram of **MODEL** algorithm



MODEL

balance of gas components:

$$\frac{dn_i}{dW} = r_i$$

pressure drop (Levy):

$$\frac{dp}{dW} = \frac{2 \cdot f_m \cdot u_g^2 \cdot \rho_g \cdot L_r \cdot (1 - \varepsilon)^{3-N}}{d_p \cdot \phi^{3-N} \cdot \varepsilon^3}$$

temperature increase by reactions:

$$\frac{dT_{r,i}}{dW} = \frac{\sum(-\Delta H_{r,i}(T) \cdot (-r_i))}{\sum(n_i \cdot c_{p,i})}$$

temperature drop by heat loss:

$$\frac{dT_{loss}}{dW} = \frac{dQ_{loss}}{m_{SUM} \cdot c_{pSUM}}$$

Fig. 5 Tested commercial **monolithic** and **bulk** catalysts

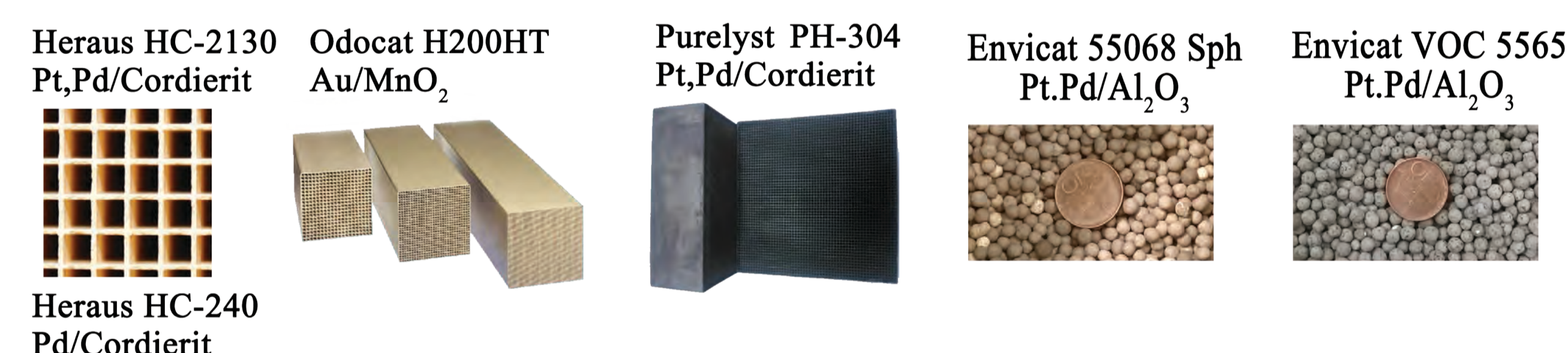


Fig. 3 Conc. of gas components, T and p

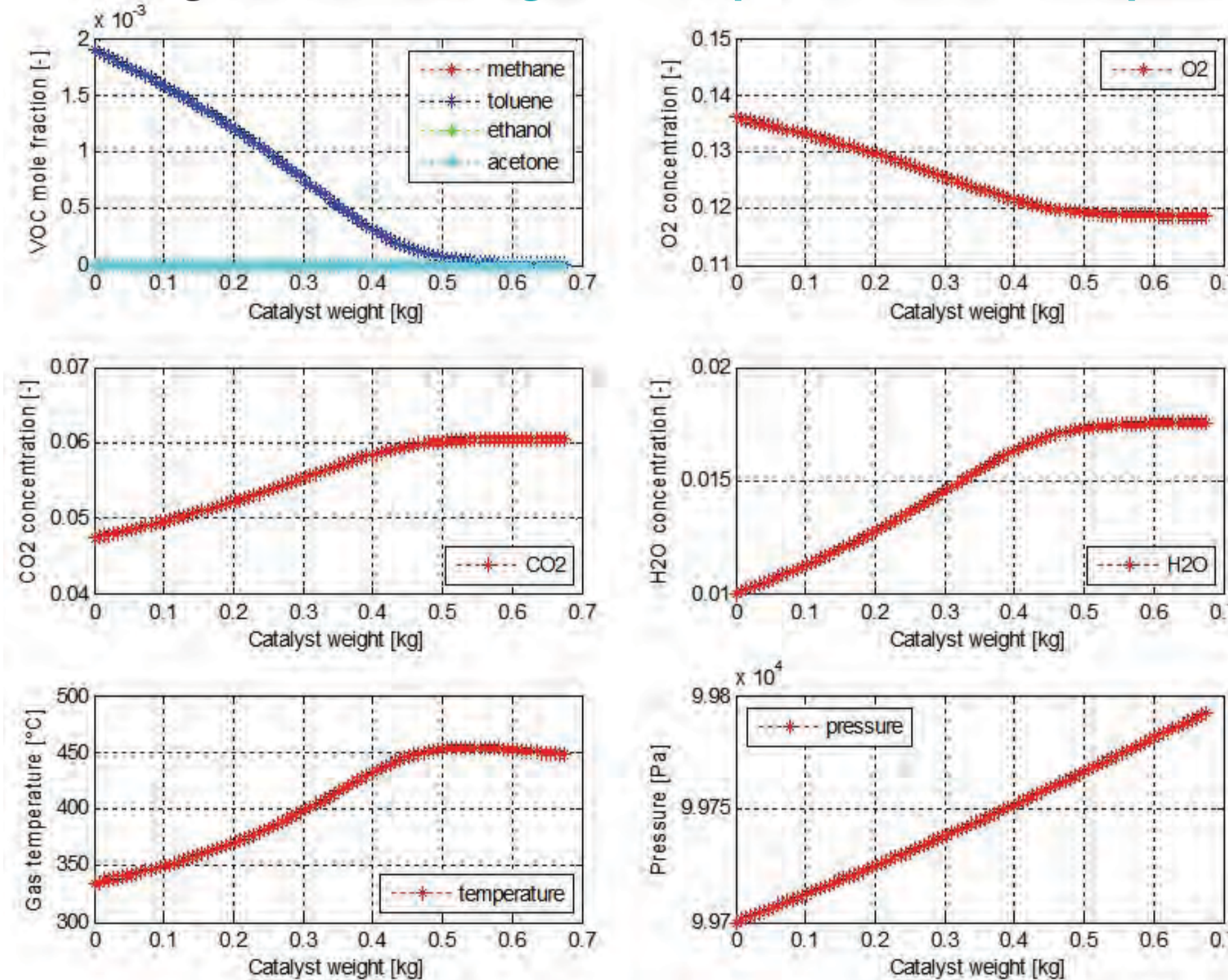


Fig. 4 Gas properties and T losses

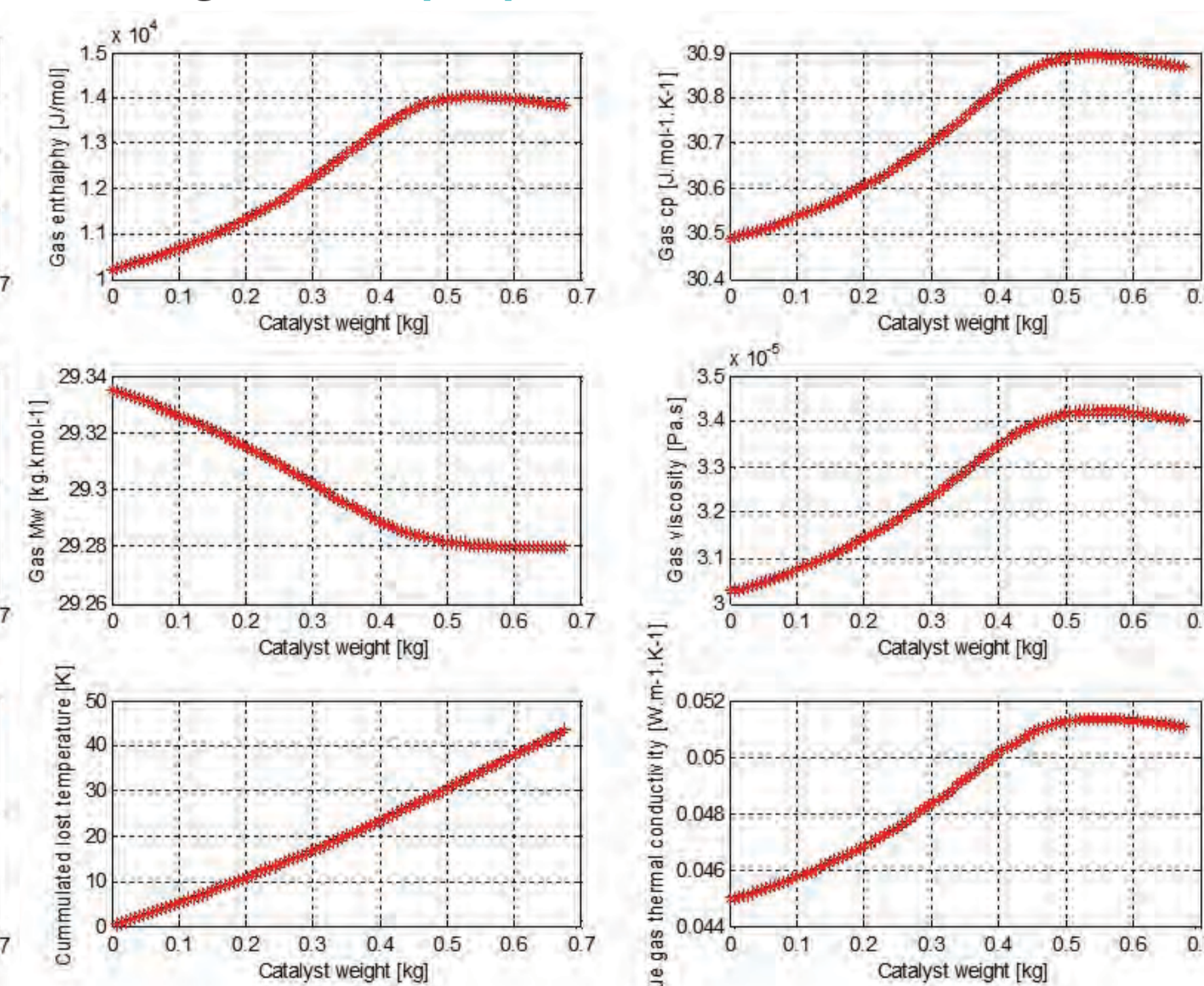


Fig. 2 Conversion and reaction rate of VOC

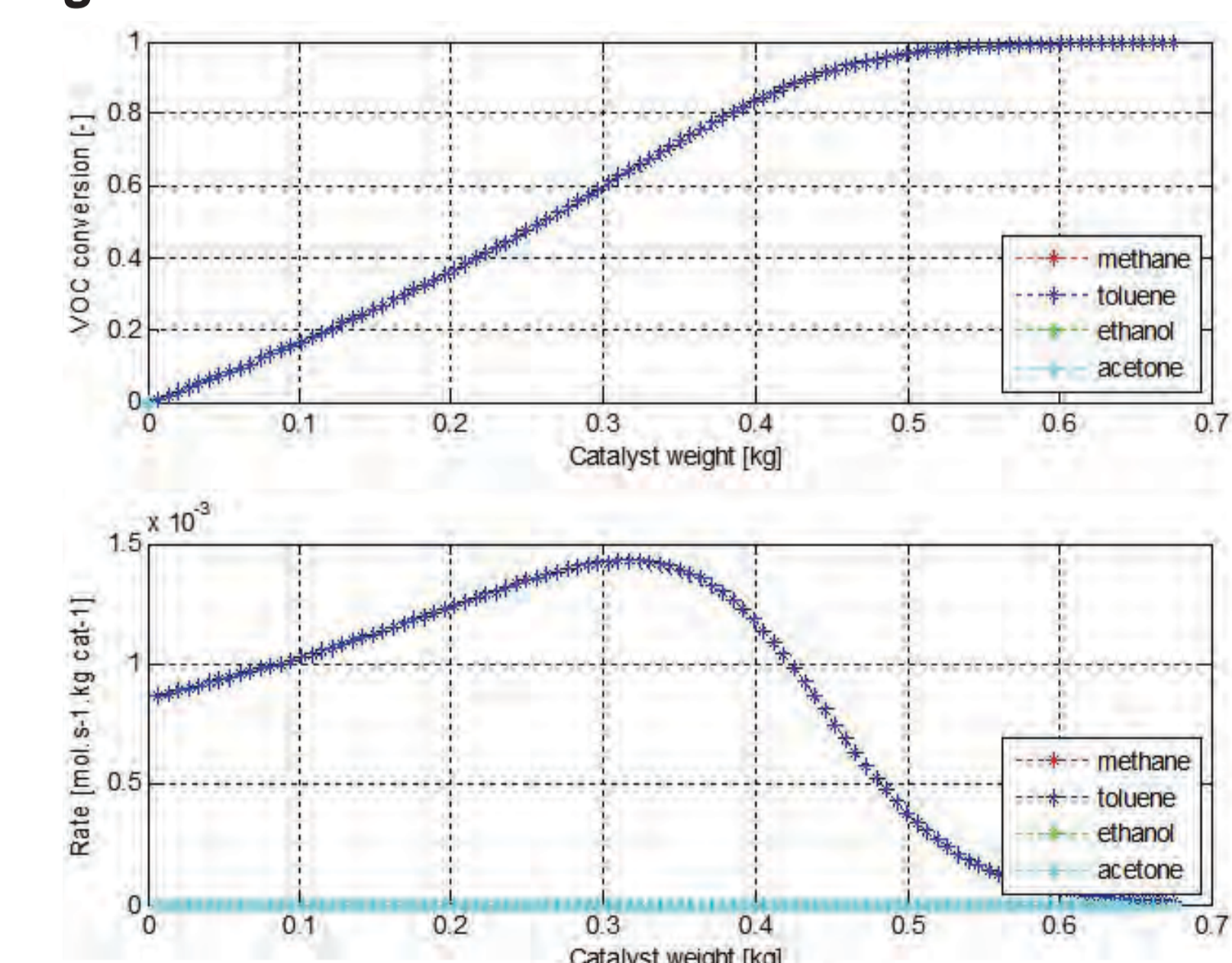
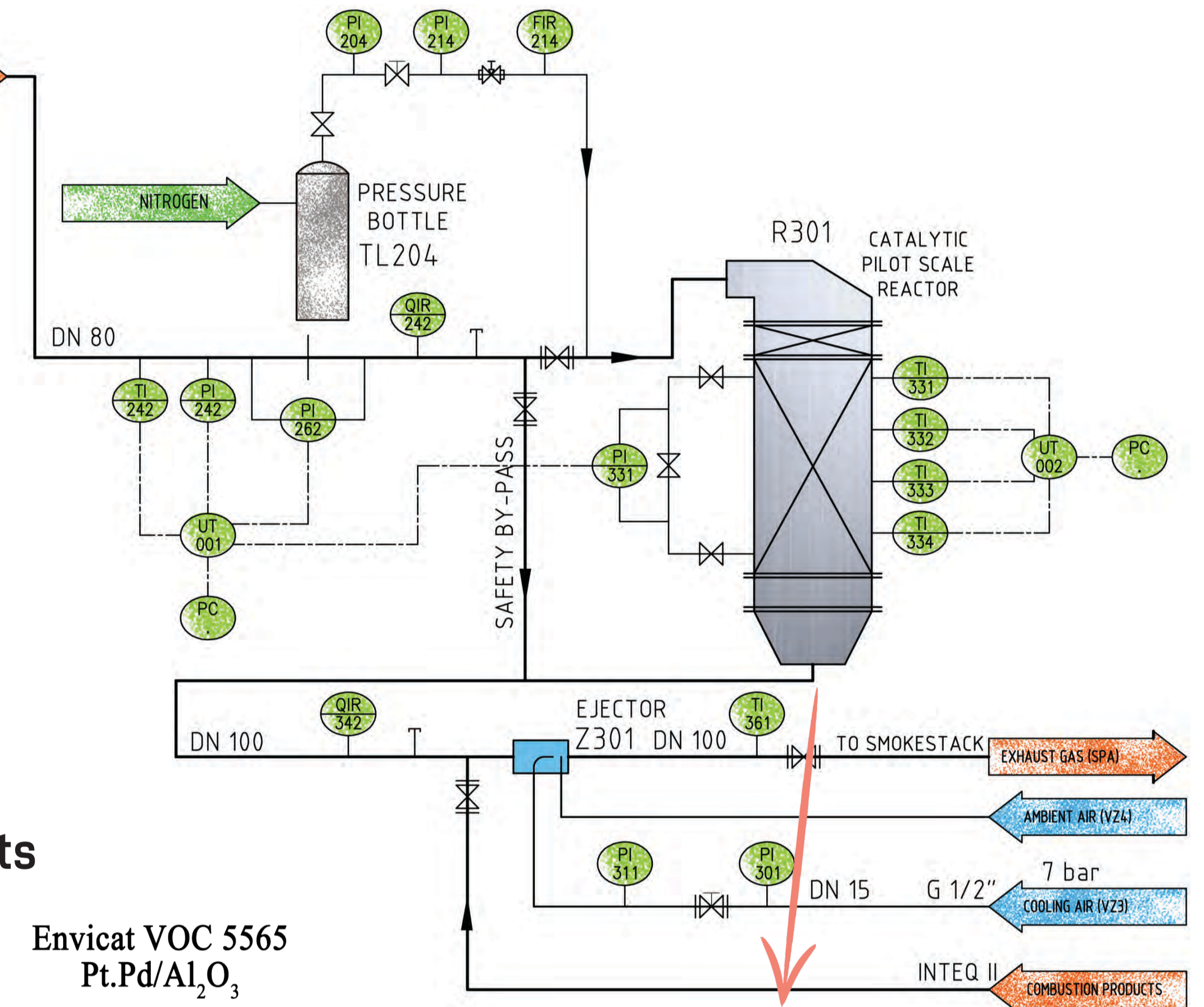


Fig. 7 Modular design - **PILOT PLANT**



Conclusions

- Modular (reactor body and in-built parts) **PILOT PLANT** was built for new types of catalysts and catalysts verification.
- PILOT** catalyst testing can significantly reduce the risk of an investment before fullscale implementation.
- A mathematical **MODEL** of a non-isothermal plug-flow reactor was developed

- for **CATOX** of selected VOC. The data obtained from the **MODEL** were compared with experimental data acquired from the **PILOT PLANT**.
- Good agreement of data - model vs experiment for the test case (VOC conversion + 2% rel. dev., T_{out} of + 3% rel. dev., Δp of the bed - 62% rel.
- Reactor **MODEL (PILOT)** - it is not possible to neglect the heat losses of the reactor structures (43 K T_{out} difference - M vs P in test case if neglected)

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