

TiAl6V4 bistable mechanism produced by Laser Powder Bed Fusion

Jan Jaroš, Matěj Duchoň, Daniel Vícha, Václav Pchálek, Čeněk Šváb, Daniel Koutný

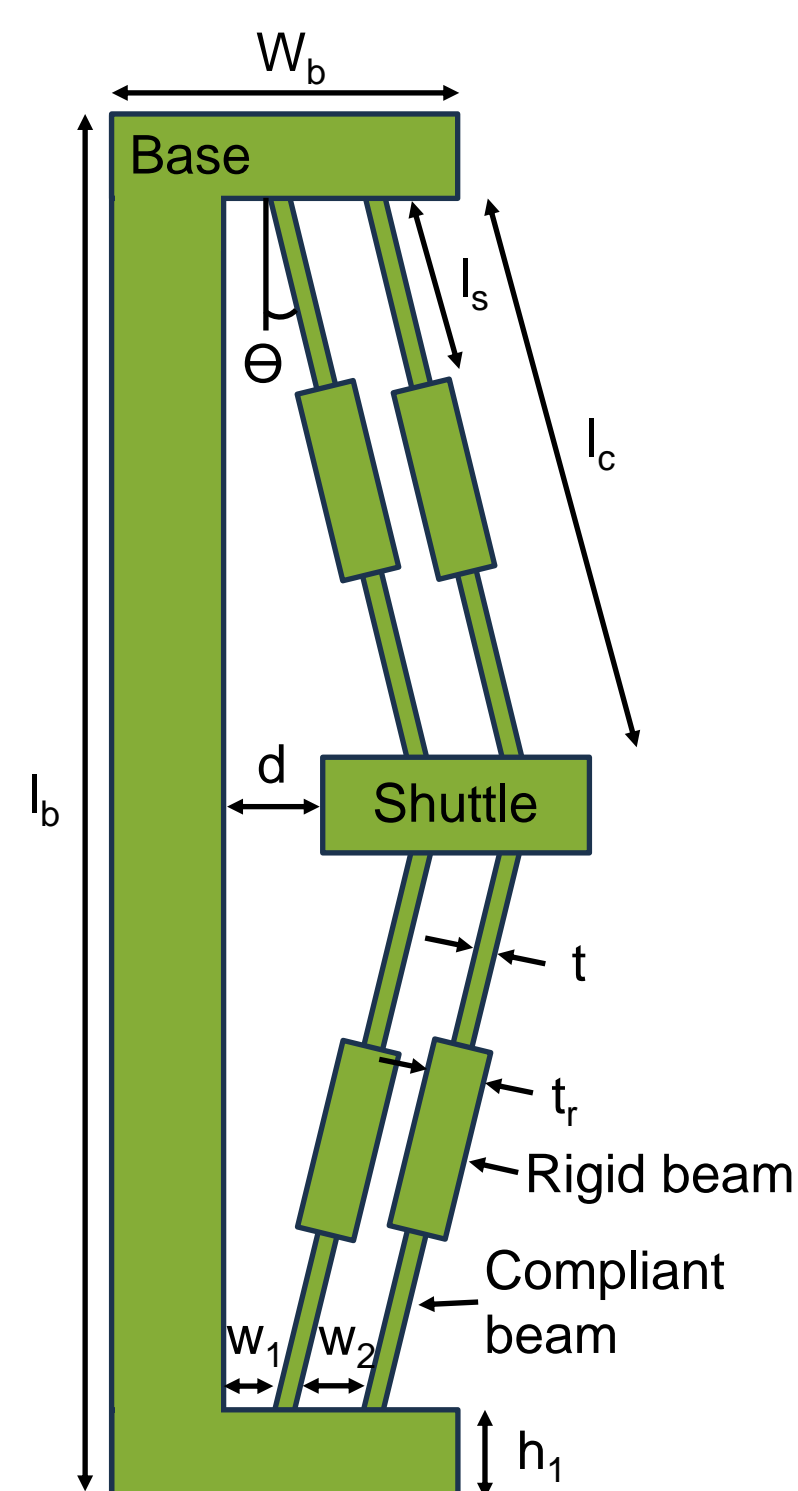
Faculty of Mechanical Engineering, Institute of Machine and Industrial Design, Brno University of Technology, Technicka 2896/2, 616 69 Brno, Czech Republic

MOTIVATION

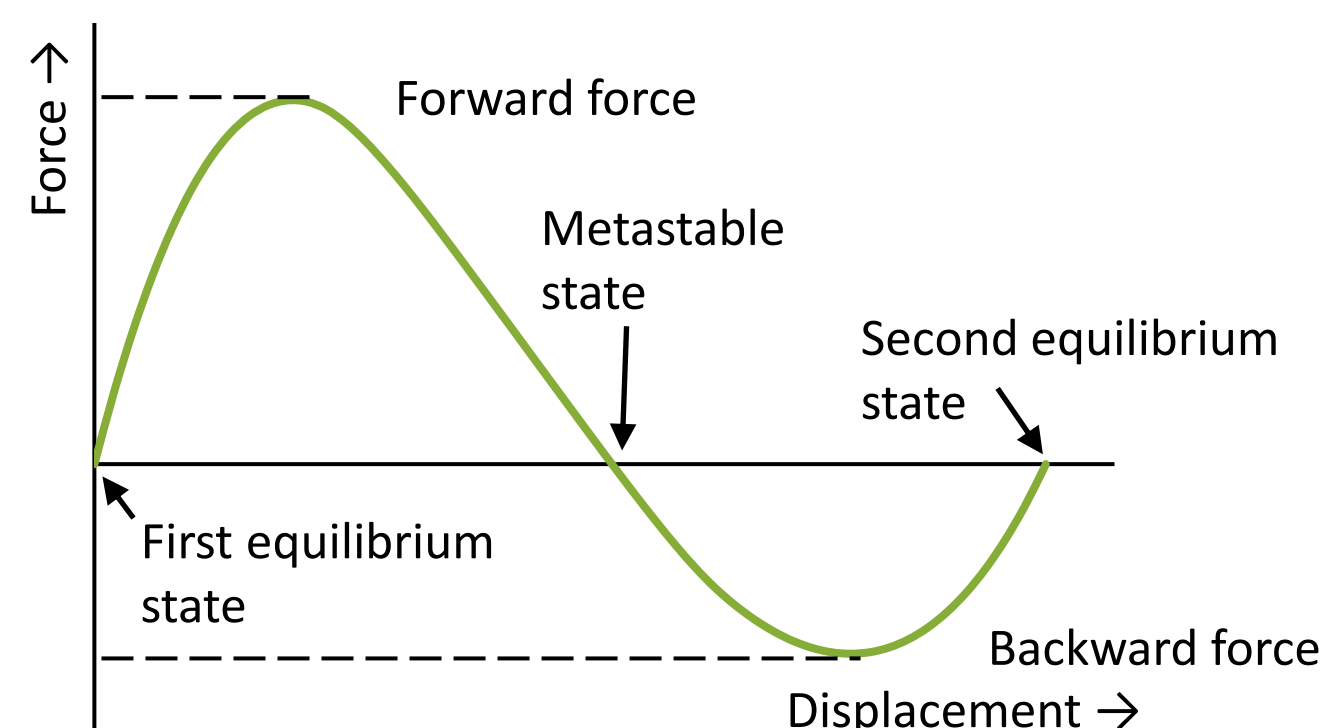
- Mechanism for compliant wing actuation
- Two equilibrium states without the need for external energy supply
- Elastic deformation that eliminates friction
- Suitable for many applications such as switches, grippers, energy harvesters and soft actuators [1-6]

THEORY

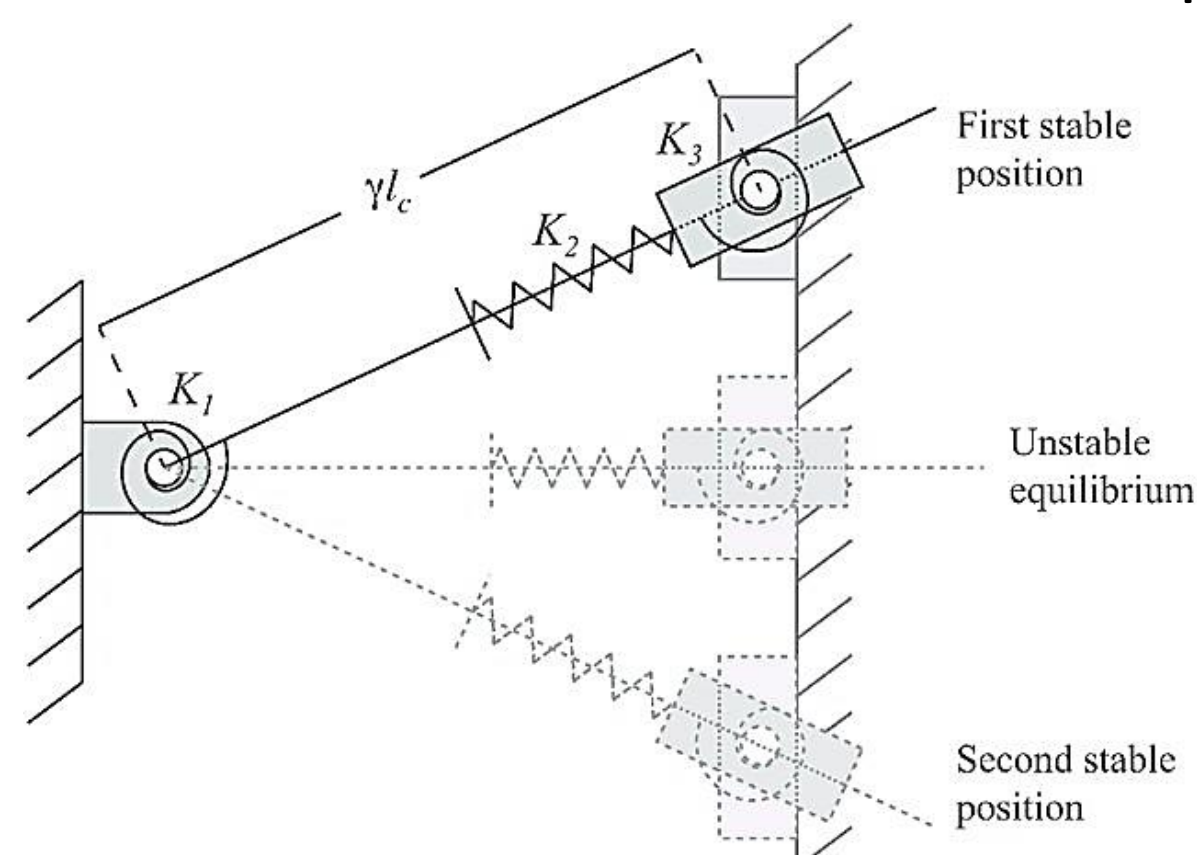
- Geometry of a compliant bistable mechanism



- Typical force-displacement response



- Analytical pseudo-rigid-body model of the compliant mechanism for the displacement and rough approximation for the stress [7]
- The compliance of the mechanism is defined by torsional and linear springs [7]
- Limitation for only compliant beams (without rigid beams that increase the force response)



$$K_1 = K_3 = \frac{2\gamma K_\theta EI}{l_c}$$

$$K_2 = \frac{3EI_b}{w_1^3}$$

$$K_\theta = 2.67617$$

$$\gamma = 0.8517$$

$$I = bt^3/12$$

$$I_b = bh_1^3/12$$

REFERENCES

1. Yan, L. et al. Applied Sciences (Switzerland) 13, (2023)
2. Liu, M. et al. Micromachines 13, (2022)
3. Chang, P. L. et al. Mech Mach Theory 152, (2020)
4. Chen, K. et al. Mech Syst Signal Process 188, (2023)
5. Li, B. et al. Advanced Intelligent Systems 4, (2022)
6. Howell, L. L. et al. (John Wiley & Sons, 2013)
7. Zirbel, S. A. et al. PLoS One 11, (2016)

RESEARCH OBJECTIVE

Design and manufacture of a bistable mechanism capable of maintaining a load of 175 N in the second equilibrium state

- Laser powder bed fusion process to produce a bistable mechanism from a TiAl6V4 alloy
- The base of the mechanism is machined with defined dimensions

l_b (mm)	w_b (mm)	h_1 (mm)	w_1 (mm)	w_2 (mm)
164	60	15	16.5	3.4

RESEARCH PLAN

FEA of the bistable mechanism with rigid beams

- 2D representation
- Default parameters with one parameter variable
- Force and stress response to identify the influence of the variable parameters

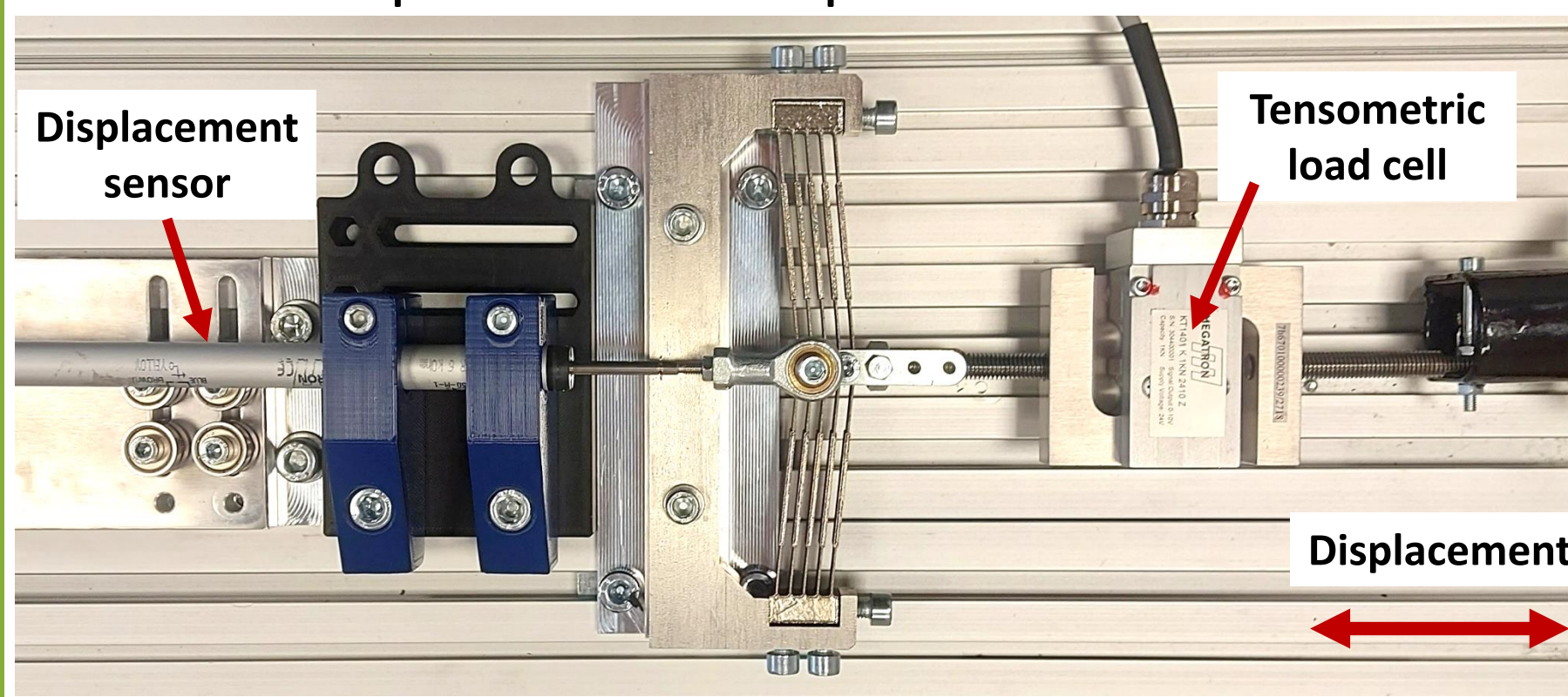
	Beams	θ	l_s	t	t_r
	(-)	(°)	(mm)	(mm)	(mm)
Default p.	3	95	15	0.6	1.5
Variable p.	1-5	92-98	10-20	0.4-1	1-2

FEA of the final bistable mechanism

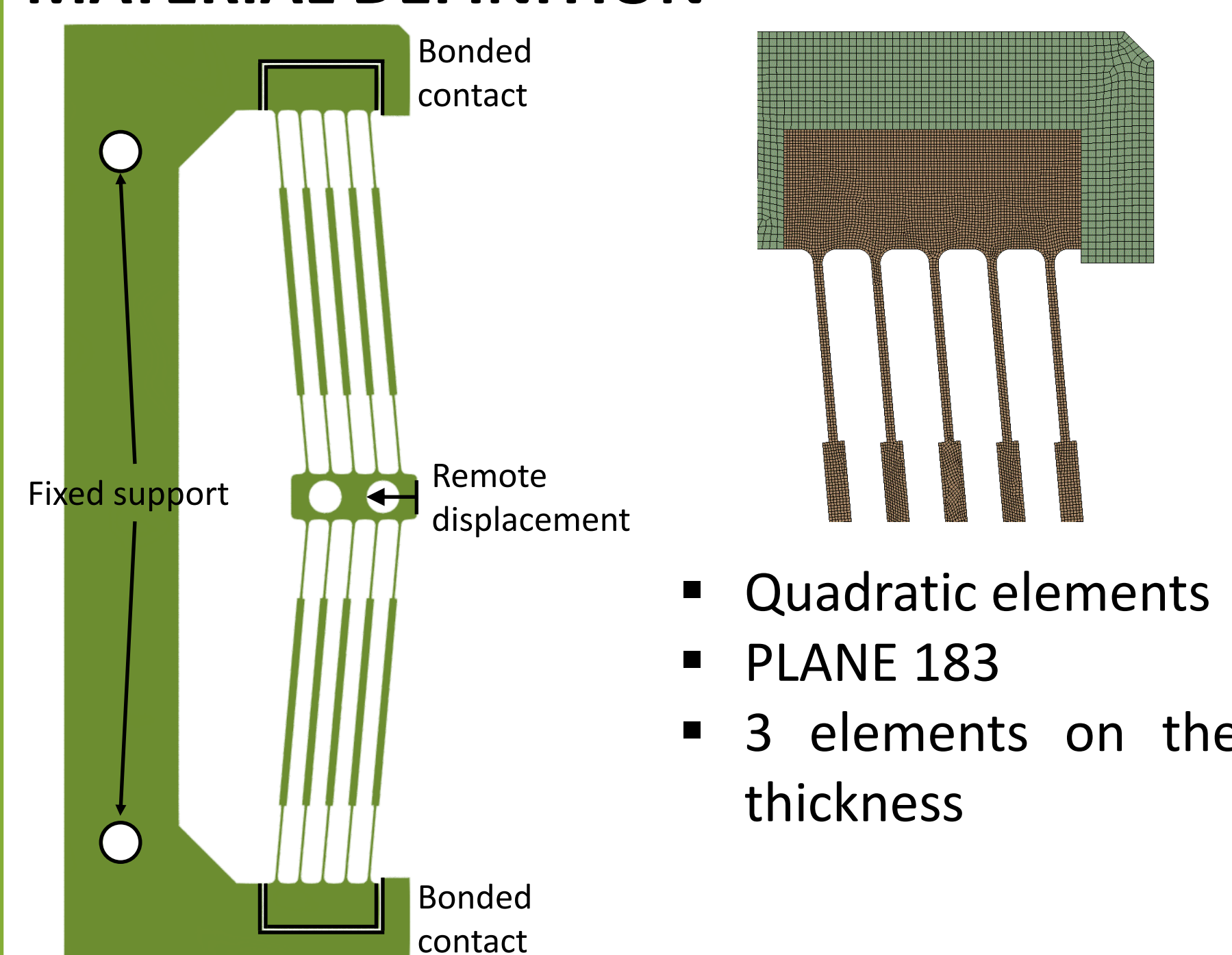
- Material defined based on the lamellas tested in bending with a thickness of 0.6 mm tested in bend (established production)
- Force and stress response

Experimental measurement of the final bistable mechanism

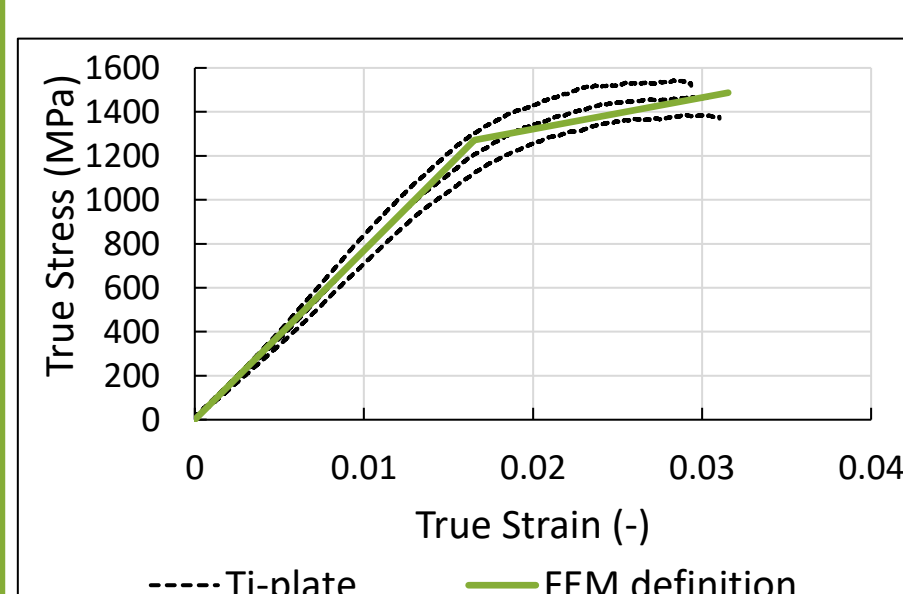
- Force response for comparison with FEA



FEA BOUNDARY CONDITIONS AND MATERIAL DEFINITION

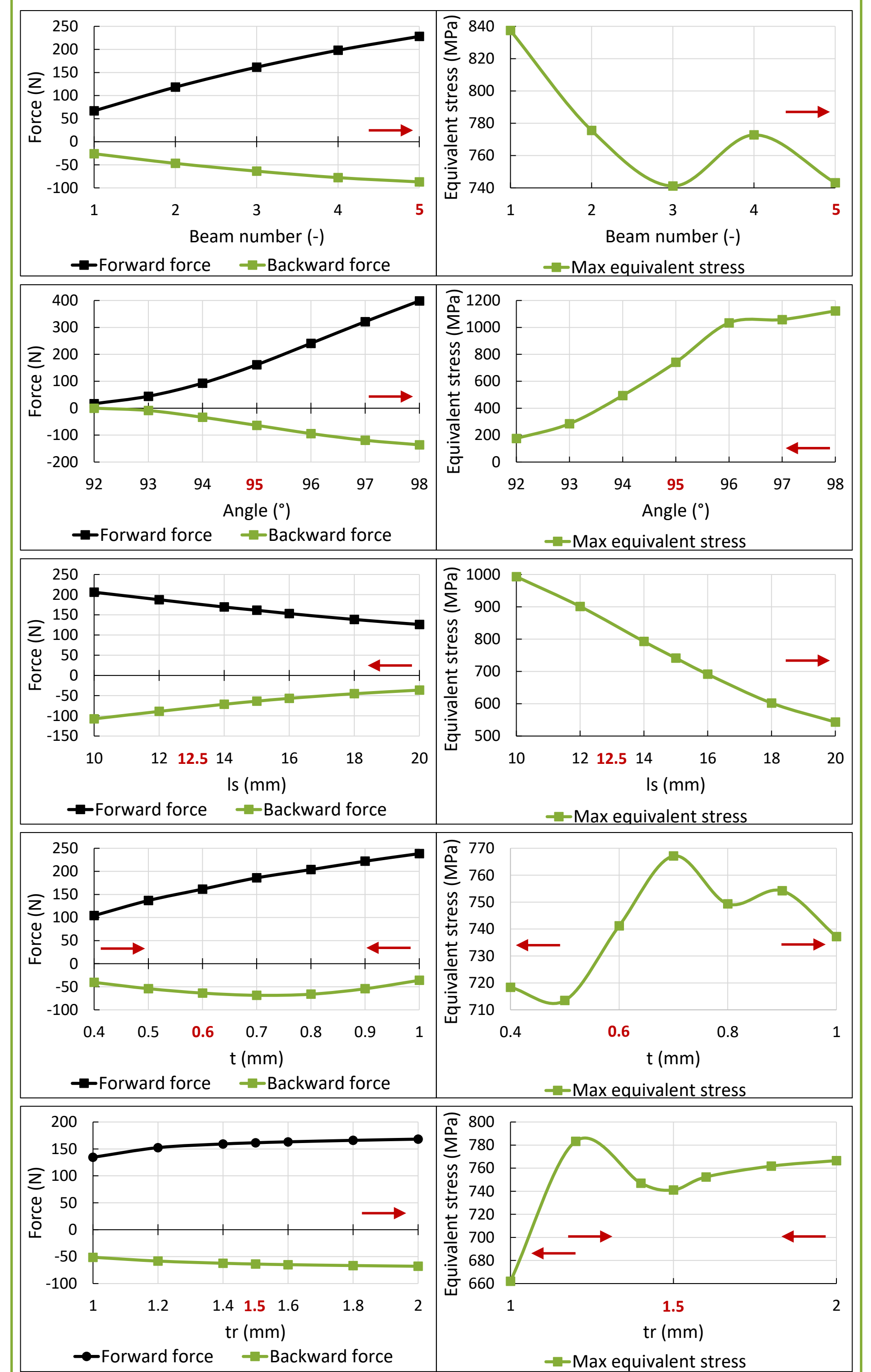


- Bilinear material definition
- $E = 76.9$ GPa,
- $Re = 1272$ MPa,
- $\nu = 0.36$



RESPONSE OF THE BISTABLE MECHANISM PARAMETERS

- Identify the parameters that increase the backward force and lead to low equivalent stress



FINAL BISTABLE MECHANISM

Geometry

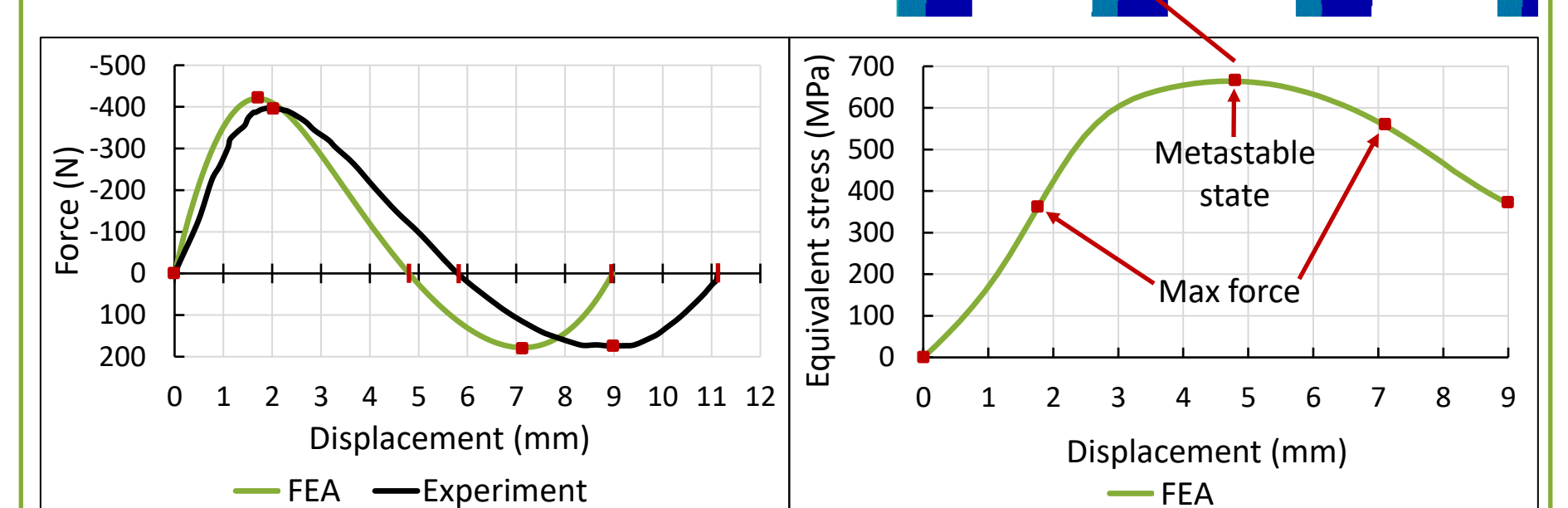
Beams	θ	l_s	t	t_r
(-)	(°)	(mm)	(mm)	(mm)
5	95	12.5	0.6	1.5

Backward force

- FEA 177.77 N
- Experiment 173.85 N

Maximum stress

- FEA 664.29 MPa



CONCLUSION

- The experimental data showed a very good agreement with FEA for forces (5.3% and 2.2%)
- The displacement showed a deviation of the experiment from the FEA (1 mm and 2.17 mm)
- The safety factor for the material was 1.91



Funded by the European Union